Adaptive optoelectronic camouflage systems with designs inspired by cephalopod skins

Cunjiang Yu\textsuperscript{a}, Yuhang Li\textsuperscript{b,c}, Xun Zhang\textsuperscript{d}, Xian Huang\textsuperscript{d}, Viktor Malyarchuk\textsuperscript{d}, Shudao Wang\textsuperscript{d}, Yan Shi\textsuperscript{b,e}, Li Gao\textsuperscript{d}, Yewang Su\textsuperscript{d}, Yihui Zhang\textsuperscript{h}, Hangxun Xu\textsuperscript{i,1}, Roger T. Hanlon\textsuperscript{b,h}, Yonggang Huang\textsuperscript{g}, and John A. Rogers\textsuperscript{d,i,1}

*Department of Mechanical Engineering, Department of Electrical and Computer Engineering, University of Houston, Houston, TX 77204; \textsuperscript{b}Department of Civil and Environmental Engineering, Department of Mechanical Engineering, Center for Engineering and Health, and Skin Disease Research Center, Northwestern University, Evanston, IL 60208; \textsuperscript{c}The Solid Mechanics Research Center, Beihang University, Beijing 100191, China; \textsuperscript{d}Department of Materials Science and Engineering, University of Illinois at Urbana–Champaign, Urbana, IL 61801; \textsuperscript{e}State Key Laboratory of Mechanics and Control of Mechanical Structures, Nanjing University of Aeronautics and Astronautics, Nanjing 210016, China; \textsuperscript{f}Department of Polymer Science and Engineering, Chinese Academy of Sciences Key Laboratory of Soft Matter Chemistry, University of Science and Technology of China, Hefei 230026, China; \textsuperscript{g}Marine Biological Laboratory, Woods Hole, MA 02543; \textsuperscript{h}Department of Ecology and Evolutionary Biology, Brown University, Providence, RI 02912; and \textsuperscript{i}Department of Electrical and Computer Engineering, Department of Mechanical Science and Engineering, Frederick Seitz Materials Research Laboratory, and Beckman Institute for Advanced Science and Technology, University of Illinois at Urbana–Champaign, Urbana, IL 61801

Edited by David A. Weitz, Harvard University, Cambridge, MA, and approved July 30, 2014 (received for review June 5, 2014)

Octopus, squid, cuttlefish, and other cephalopods exhibit exceptional capabilities for visually adapting to or differentiating from the coloration and texture of their surroundings, for the purpose of concealment, communication, predation, and reproduction. Long-standing interest in and emerging understanding of the underlying ultrastructure, physiological control, and photonic interactions has recently led to efforts in the construction of artificial systems that have key attributes found in the skins of these organisms. Despite several promising options in active materials for mimicking biological color tuning, existing routes to integrated systems do not include critical capabilities in distributed sensing and actuation. Research described here represents progress in this direction, demonstrated through the construction, experimental study, and computational modeling of materials, device elements, and integration schemes for cephalopod-inspired flexible sheets that can autonomously sense and adapt to the coloration of their surroundings. These systems combine high-performance, multiplexed arrays of actuators and photodetectors in laminated, multilayer configurations on flexible substrates, with overlaid arrangements of pixelated, color-changing elements. The concepts provide realistic routes to thin sheets that can be conformally wrapped onto solid objects to modulate their visual appearance, with potential relevance to consumer, industrial, and military applications.

Significance

Artificial systems that replicate functional attributes of the skins of cephalopods could offer capabilities in visual appearance modulation with potential utility in consumer, industrial, and military applications. Here we demonstrate a complete set of materials, components, fabrication approaches, integration schemes, bioinspired designs, and coordinated operational modes for adaptive optoelectronic camouflage sheets. These devices are capable of producing black-and-white patterns that spontaneously match those of the surroundings, without user input or external measurement. Systematic experimental, computational, and analytical studies of the optical, electrical, thermal, and mechanical properties reveal the fundamental aspects of operation, and also provide quantitative design guidelines that are applicable to future embodiments.


The authors declare no conflict of interest. This article is a PNAS Direct Submission.

To whom correspondence should be addressed. Email: jrogers@illinois.edu.

1To whom correspondence should be addressed. Email: jrogers@illinois.edu.

This article contains supporting information online at www.pnas.org/lookup/suppl/doi:10.1073/pnas.1410494111/-/DCSupplemental.
ranges from ca. 250 to 750 ms. The middle and bottom layers are composed of structural coloration components. The middle layer comprises iridophore cells that can reflect all colors depending on angle of view; some are passive cells and others are physiologically controlled by a slower system: They can be turned on/off in 2–20 s (depending on species, or different cell types on different parts of the body). The bottom layer comprises leucophores (i.e., “white cells”) that are entirely passive (i.e., no physiological control; they are always “on”). This layer diffuses white in all directions (25) and can act as a bright backdrop.

**Fig. 1.** Schematic illustrations and images of adaptive camouflage systems that incorporate essential design features found in the skins of cephalopods. (A) Exploded view illustration of a single unit cell that highlights the different components and the multilayer architecture. The first and second layers from the top correspond to the leucodye composite (artificial chromatophore; ac) and the Ag white reflective background (artificial leucodye; al). The third layer supports an ultrathin silicon diode for actuation, with a role analogous to that of the muscle fibers that modulate the cephalopod’s chromatophore (artificial muscle; am). The bottom layer, separated from the third layer by PDMS, provides distributed, multiplexed photodetection, similar to a postulated function of opsin proteins found throughout the cephalopod skin (artificial opsin; ao). (B) Optical image of a thermochromic equivalent to a chromatophore. (C) Optical micrograph of the Ag layer and the silicon diode. (D) Optical image of the diode. (E) Optical image of a photodiode and an associated blocking diode for multiplexing. (F) Exploded view of illustration of a 16 × 16 array of interconnected unit cells in a full, adaptive camouflage skin. (G) Top view image of such a device. (H) Image of the region highlighted by the red box in G. (I) Image of a device in a bent configuration.
against which expanded pigmented chromatophores are viewed; this provides one way in which contrast of the pattern can be controlled (i.e., darkly pigmented chromatophores next to bright white reflective elements).

The central control of skin patterning resides in the eyes, which, together with the central and peripheral nervous system, sense the visual background and route control signals throughout the skin to produce a coordinated pattern for communication or camouflage. In addition, the skin contains molecules known as opsins, which are known to be photosensitive in the retina and are thought to be photosensitive in the skin as well. They are hypothesized to play a role in distributed light sensing and control in the periphery (26), thus potentially adding a non-centralized component for skin patterning that enables sensing and actuation independent of the brain.

One of the most important features of cephalopod skin—one that provides maximum optical diversity of appearances—is the coordinated action of (i) chromatophores, (ii) iridophores, (iii) leucophores, (iv) muscles, (v) central ocular organs, and (vi) distributed opsins (2, 23–25). The work described here demonstrates pixelated devices that include analogous to each of these key elements, except for the second and fifth, which can be easily incorporated with known photonic materials and conventional digital imagers.

Results

Fig. 1A presents a schematic illustration of a unit cell; the multilayer stack includes, from top to bottom, a color-changing element (analogous to a chromatophore) on top of a white reflective surface (analogous to a leucophore), an actuator (analogous to the muscles that control the chromatophore), and a light sensor (analogous to a functional unit involving opsins), all on a flexible plastic support. Optical images illustrate the materials and device structures used for each of these components: microencapsulated thermochromic dye embedded in a photopatterning polymer matrix (Fig. 1B) to define the color, a thin layer of silver (Ag) to create a bright white background (Fig. 1C), an ultrathin silicon (Si) diode to provide multiplexed Joule heating for control over the optical properties of the dye (Fig. 1D), and an ultrathin Si photodiode and blocking diode, also configured for multiplexing, to yield a control signal (Fig. 1E). A complete system consists of a 16 × 16 array of such unit cells, in the form of a flexible skin (1.4 cm × 1.4 cm), as illustrated schematically in Fig. 1F and in the images of Fig. 1G and H. The thin geometries of the active components and the compliance of the polydimethylsiloxane (PDMS; 100 μm thick; ~2 MPa modulus) substrate lead to high levels of mechanical flexibility (Fig. 1F).

The artificial chromatophores incorporate a thin layer of microencapsulated leucodye (black 47°C, LCR Hallcrest) embedded in a photosensitive transparent polymer (SU-8 50, Microchem). The dye is based on a fluoran chemistry that reversibly converts from open (colored) to closed (colorless) form lactone rings upon temperature cycling below and above 47 °C, respectively. This composite combines abilities for color modulation via the leucodye (27–29) with photopatterning via the transparent polymer matrix. An example of a black (transparent) slurry of this composite at 22 °C (47 °C) is shown in SI Appendix, Fig. S1A and B. Crosslinking by patterned exposure to UV light allows unexposed regions to be washed away, thereby yielding pixelated patterns (thicknesses of ~65 μm and edge resolution of 10 μm) such as those shown in Fig. 1B. The notched corners create openings for light sensing by photodetectors located at these positions. Details appear in SI Appendix, including scanning electron microscope images in SI Appendix, Fig. S1.

The results from an artificial chromatophore of this type at 22 °C and 47 °C are shown in SI Appendix, Fig. S1 E and F. Here, a thin layer of Ag, also patterned into a pixelated geometry, serves as an artificial leucophore to provide a bright white reflective background. Corresponding spectral reflectance properties appear in Fig. 2D as a function of temperature. The reflectance can be further improved by use of strongly scattering materials (e.g., titania nanoparticles) and/or thermochromic materials with improved transmittance in their transparent state.

Fig. 2. Photodetection and color switching. (A) Optical reflectance measured throughout the visible range and at normal incidence from a layer of a thermochromic composite on a white Ag film, at 20 °C (black) and 47 °C (white). (Inset) The cross section of the structure. (B) I-V characteristics of a multiplexed diode for actuation, measured at temperatures between 20 °C and 70 °C, with an increment of 10 °C. (C) I-V characteristics of a multiplexed photodetector measured while under white light illumination (light on, red) and in the dark (light off, black). (D) Measured (IR image; top) and computed (3D FEM; bottom) distributions of temperature associated with a device during multiplexed actuation of a single unit cell located in the center. (E) Time-dependent variations in temperature at the center of a unit cell during multiplexed actuation that begins at ∼11 s and ends at ∼41 s. The black dots are experimental data extracted from movies recorded using an IR camera. The red curve represents FEM results. (F) Experimental and FEM results for times between −18 s and −23 s. The minimum and maximum temperatures are −47 °C and −62 °C, respectively.
This color changing strategy offers viewing-angle-independent appearance and a simple, thermal switching mechanism, suitable for present demonstration purposes. The high thermal conductivity of the Ag layer is important for this latter feature, as described subsequently.

Selective actuation of these photodefined chromatophores/leucophores yields programmable patterns of black and white. An array of ultrathin (total thickness ~10 μm; bending stiffness per length ~1.7 μN) Si diodes (single crystal Si 640 × 640 μm² in area, 1.25 μm thick) provides local heating for this purpose, with multiplexed addressing (SI Appendix, Fig. S2). Details of the fabrication and optical images of representative devices appear in SI Appendix, Figs. S3, S4, and S2C, respectively. The yields are >95%. Fig. 2B presents the current-voltage (I-V) characteristics of a typical device (forward voltage ~0.7 V; current ~190 mA at a forward bias of 10.5 V). The properties are independent of temperature over this range, thereby ensuring stable behavior in all relevant operating modes presented here. Multiplexed addressing involves application of power in a pulsed mode, with row/column scanning. The designs of the external electronics for this purpose are summarized in SI Appendix, Figs. S5 and S6. The ability to localize heating to a single unit cell in this manner is demonstrated in SI Appendix, Fig. S2D.

Distributed sensing of background patterns is achieved via artificial opsins that consist of photodiodes and multiplexing switches. The materials and fabrication schemes for these components are similar to those of the Joule heating elements described above. (Details appear in SI Appendix.) The responses of the photodetectors define the pattern of thermal actuation and, therefore, the resulting patterns of coloration. As illustrated in Fig. 1E and SI Appendix, Figs. S7A and B, each unit cell includes a photodiode and a multiplexing (blocking) diode connected in a back-to-back fashion. These devices are positioned at the notches in the patterned chromatophore/leucophore pixels to allow exposure to light incident on the system from above or below. The blocking diode incorporates an opaque coating to eliminate its sensitivity to light. The I-V curves of the photodetector in dark and light conditions appear in Fig. 2C, where the dark current is ~1 nA and the photocurrent is ~1 μA. The yields are ~100%. A digital image that results from patterned illumination appears in SI Appendix, Fig. S8A and B. A binarized intensity distribution derived from such an image serves as a control signal to establish closed-loop operation of the entire system. The actuation and sensing layers have excellent flexibility (SI Appendix, Figs. S4D and S7C) due to their thin construction. No delamination occurs even when the integrated device was bent to a radius of 2 mm. Finite element modeling (FEM) results for bending to this degree appear in SI Appendix, Fig. S12A. The same geometry allows separate fabrication of these layers and subsequent lamination of them on top of one another to form a complete system (SI Appendix, Fig. S9). The lamination process occurs at the wafer scale, with the potential for use over larger areas with proper tooling and alignment procedures. This type of integration allows separate fabrication of the various subsystems, thereby improving the overall device yields, to levels of >95%. Images of the device before and after integrating the Ag layers are shown in SI Appendix, Fig. S10A and B. Thin flexible cables based on anisotropic conductive films bond to electrode pads at the periphery for electrical connection to external power supply and analysis hardware, as in SI Appendix, Fig. S11.

Multiplexed photodetection and coordinated actuation are central to the overall operation. Responses of the diodes under pulsed mode voltages between 5.5 V and 12.5 V yield insights into the mechanisms of heating and thermal diffusion. Measurements under these conditions involve digital image capture of color changes in the chromatophore, simultaneously with temperature evaluation using an infrared (IR) camera (A655SC, FLIR Systems, Inc.). The minimum operating voltage is defined by initiation of color change at the location of the targeted pixel; the maximum is defined by onset of change in adjacent pixels, via thermal diffusion. As shown in SI Appendix, Figs. S13 and S14, typical minimum and maximum voltages are ~10.5 V and ~11.5 V, respectively. All system tests reported here used values near the minimum. Fig. 2D illustrates measured (top) and computed (bottom) distributions of temperature during operation of a single, isolated pixel. The multiplexing scheme naturally leads to fluctuations in temperature about a baseline level, as shown in the experimental (black dots) and 3D FEM results (red lines) of Fig. 2E and F, and SI Appendix, Fig. S15. Here, the applied power begins and ends at 11 s and 41 s, respectively. The pulses have a duration of t₀ = 17.5 ms and a period of T = 280 ms. The color changes from white to black after ~1 s, corresponding to four pulses. Results of SI Appendix, Fig. S15B, indicate that the temperature increases sharply and then fluctuates between 47 °C and 60 °C, after stabilization. A key finding is that changes in

![Fig. 3. Illustration of metachrosis for several different static patterns. Top view image of the device in a uniform geometry (A), in a triangular pattern (B), and in an array of small (C) and large (D) squares. (E) Image of a device in operation while bent, while showing the text pattern “U o I”.

Yu et al. PNAS | September 9, 2014 | vol. 111 | no. 36 | 13001
temperature remain confined largely to a single pixel, without significant diffusion to neighboring pixels. The lateral uniformity and pixel-level localization of the changes in temperature follow from (i) the high thermal conductivity of the Ag layer and its ability to facilitate thermal diffusion from the diode source and (ii) the pixelated pattern of this material and the leucodye composite. The temperature is nearly constant throughout the depth of this composite, due to its thin geometry. These collective features enable arbitrary pattern generation to a resolution set by the numbers of pixels and their sizes. An example of a pattern of the character “O” appears in Movie S1 (experimental results) and Movie S2 (modeling results).

Experimental procedures used to study camouflage capabilities in cuttlefish (2, 30–33) serve as a model for illustrating full function, i.e., metachrosis, of the systems. Here, a device rests on a patterned black-and-white background formed by passing white light through an amplitude mask from below. External control electronics automatically send signals to the actuators at locations where responses from associated photodetectors exceed a threshold. Fig. 3A shows a case in which all pixels turn white, consistent with the uniformly bright pattern of the background. Different static geometries, including triangles,
arrays of dots, and even random patterns, can be achieved, with either flat or curved configurations, as shown in Fig. 3 B–E.

Dynamic pattern recognition and matching are also possible, as illustrated in Fig. 4 A and B. In this case, changing the position of an amplitude mask that passes light only through a small square region leads to corresponding changes in the displayed patterns (Fig. 4). In these images and others of Fig. 4, the top illuminations correspond to schematic, angled view renderings of the mask and the device; the images directly below are top views of the device. Movies S3 and S4 show additional details and examples. The metachrosis process occurs within 1 or 2 s in all cases, which is similar to neutrally controlled pattern change in cephalopods (2).

Discussion

These systems establish foundations in materials science and engineering design that address key challenges in distributed sensing, actuation, and control in adaptive camouflage. The sensors and actuators provide operation across the full visible spectrum and allow for electric-field– or current-induced switching, respectively. As a result, these ideas can be applied not only with simple thermochromic materials but also with more advanced alternatives that offer improved power efficiency, facile routes to control, and robust operation without sensitivity to environmental conditions. Furthermore, the overall architecture can accommodate integration of tunable analogs to iridophores, thereby providing a vehicle for future investigations. In all cases, compatibility with large-area electronics holds promise for scalable manufacturing. Ability to reproduce physical texture, as in many cephalopods (34), remains as an interesting and challenging topic for research.

Materials and Methods

Fabrication and Assembly. Detailed fabrication procedures for the various individual components of the system appear in SI Appendix. The assembly process involves a series of lamination processes. First, a slab of PDMS (Sylgard 184, Dow Corning) was used to retrieve an interconnected array of multiplexed silicon diodes after release from a glass substrate. Exposing a separate layer of PDMS (100 μm, on a glass substrate) to UV-induced ozone (BHK, Inc.) generated a hydroxyl-terminated surface for bonding via condensation reactions with similar chemistry associated with a layer SiO₂ blanket deposited onto the array. The Ag (thickness 300 nm) and the thermochromic composite (thickness ∼65 μm) were lithographically patterned on top of the diode array. Alignment followed a scheme shown in SI Appendix, Fig. S10C. The resulting system, with the PDMS layer, was then peeled from the glass. Similar bonding processes enabled aligned integration of a separately fabricated multiplexed array of photodetectors onto the backside of the PDMS, through the use of modified mask aligner (MJB-3, Karl Suss) with alignment accuracy of 1 μm. Details appear in SI Appendix, Fabrication and assembling the complete system and Fig. S9.

Control and System Operation. The system consists of two sets of active components, i.e., sensors and actuators, each of which functions separately and at different multiplexed scanning speeds. Closed-loop operation involves (i) acquiring digital images based on the intensity distributions extracted from responses of the 16 × 16 array of photodetectors, (ii) binarizing the intensity distribution and storing the resulting data in a buffer, and (iii) reading the buffer and addressing the 16 × 16 array of actuators by column scanning to copy the pattern, in a repeating manner. The time to acquire an image is ∼10 ms, much shorter than the pulse period for actuation (280 ms), thereby ensuring that the refresh rate of the image exceeds that of induced color change. Software development tools from LabVIEW 2012 provide all of the necessary means for implementation of the described operation.

ACKNOWLEDGMENTS. Jeff Grau is acknowledged for his help in preparing photomasks. The work on material design and device fabrication was supported by Office of Naval Research under Grant N00014-10-1-0989. C.Y. acknowledges the start-up funding support from the Department of Mechanical Engineering, Cullen College of Engineering, and the Division of Research at the University of Houston. R.T.H. also acknowledges partial support from Air Force Office of Scientific Research Grant FA9550–09–0346.
Supporting Information

Adaptive optoelectronic camouflage systems with designs inspired by cephalopod skins

Cunjiang Yu\textsuperscript{a}, Yuhang Li\textsuperscript{b,c}, Xun Zhang\textsuperscript{d}, Xian Huang\textsuperscript{d}, Viktor Malyarchuk\textsuperscript{d}, Shuodao Wang\textsuperscript{d}, Yan Shi\textsuperscript{b,c}, Li Gao\textsuperscript{d}, Yewang Su\textsuperscript{b}, Yihui Zhang\textsuperscript{b}, Hangxun Xu\textsuperscript{f}, Roger Hanlon\textsuperscript{g,h}, Yonggang Huang\textsuperscript{b}, and John A. Rogers\textsuperscript{d,i,1}

\textsuperscript{a}Department of Mechanical Engineering, Department of Electrical and Computer Engineering, University of Houston, Houston, TX 77204

\textsuperscript{b}Department of Civil and Environmental Engineering, Department of Mechanical Engineering, Center for Engineering and Health, and Skin Disease Research Center, Northwestern University, Evanston, IL 60208

\textsuperscript{c}The Solid Mechanics Research Center, Beihang University, Beijing 100191, China

\textsuperscript{d}Department of Materials Science and Engineering, University of Illinois at Urbana-Champaign, Urbana, IL 61801

\textsuperscript{e}State Key Laboratory of Mechanics and Control of Mechanical Structures, Nanjing University of Aeronautics and Astronautics, Nanjing 210016, China

\textsuperscript{f}Department of Polymer Science and Engineering, CAS Key Laboratory of Soft Matter Chemistry, University of Science and Technology of China, Hefei 230026, China

\textsuperscript{g}Marine Biological Laboratory, Woods Hole, MA, 02543

\textsuperscript{h}Department of Ecology and Evolutionary Biology, Brown University, Providence, RI, 02912

\textsuperscript{i}Department of Electrical and Computer Engineering, Department of Chemistry, Department of Mechanical Science and Engineering, Frederick-Seitz Materials Research Laboratory, and Beckman Institute for Advanced Science and Technology, University of Illinois at Urbana-Champaign, Urbana, IL 61801
To whom correspondence should be addressed. E-mail: jrogers@illinois.edu.
1. Preparing the thermochromic composite and measuring its optical characteristics

Preparation of the photodefinable thermochromic composite involved mixing microencapsulated leuco dye (black 47C, LCR Hallcrest) with SU-8 50 (Microchem, USA) at a weight ratio of 1:5 to form a liquid slurry. Microcapsules contain mixtures of leuco dye with a color developer and a low melting point solvent. At low temperatures, the developer and leuco dye form a complex that favors a colored ring-open state. Upon heating, the solvent melts, and the developer and dye dissociate. In this state, the leuco dye favors a colorless, ring-closed configuration. Such transformation occurs at 47 °C in a reversible manner. Figure S1A shows an optical image of the slurry at 22 °C. Heating to a temperature above 47 °C causes the slurry to become transparent. As shown in Fig. S1B, a background picture underneath the slurry is clearly visible at temperatures above 47 °C. Standard procedures for patterning SU-8 yield pixelated arrays of this slurry with thickness defined by the spin-speed. Figures S1C and D provide SEM images of examples. Detailed fabrication steps appear below.

The optical reflectance of the color changeable pixels (Ag/composite dye) was measured using a spectrometer (Cary 5G UV-VIS-NIR) as a function of temperature. A portable thermoelectric heater/cooler (InbS1-031.021, WATRONIX, Inc.) served to control the sample temperature. A thermocouple (Fluke 233, Fluke Corporation) was used to measure the temperature.

Fabrication steps:

1. Mix leuco dye and SU-8 50 at weight ratio of 1:5.
2. Spin-coat the mixture slurry (3000rpm, 30 sec).
3. Pre-bake at 65 °C for 5 min and 95 °C for 20 min.
4. Expose to UV light under a mask aligner (Karl Suss MJB3) at a dose of 1440 mJ/cm².
5. Post-bake at 65 °C for 2 min and 95 °C for 5 min.
6. Develop in SU-8 developer (MicroChem, USA) for 6 minutes.

7. Rinse in isopropyl alcohol (IPA) and deionized (DI) water.

2. Fabricating the diode array and measuring its electrical characteristics

Figure S2A shows an exploded schematic illustration of the layout of the Si, metal and polyimide (PI) layers associated with a single pixel in the heater array. The major steps in the fabrication include retrieving a thin (1.25 μm) crystalline film of Si with pre-defined patterns of doping from a silicon-on-insulator (SOI) wafer followed by transfer printing onto a thin polyimide (PI) substrate, and then applying layers for metallization and passivation, as outlined in Figs. S3 and 4. A thin layer of gold eliminates the potential for crosstalk induced by light. Figure S2B shows the planar structure and design of the Si heater; the small dots correspond to holes introduced into the Si to facilitate chemical etching for release. The measured I-V curves at different temperatures appear in Fig. 2B. Figure S2C shows an optical image of a 16×16 array of unit cells. Individual addressing is achieved without affecting the neighborhood pixels, as evidenced by the IR image (QFI InfraScope II) of Fig. S2D. Here, the background temperature was set to 30 °C, to facilitate IR imaging. Detailed fabrication steps are as follows.

Fabrication steps:

Defining alignment markers

1. Clean 1.25 μm SOI wafer (acetone, isopropyl alcohol (IPA), deionized (DI) water).

2. Pattern photoresist (PR; Clariant AZ5214, 3000 rpm, 30 sec) with 365 nm optical lithography (Mask #1: Alignment marker).

3. Etch Si by RIE (50 mTorr, 40 sccm SF₆, 100 Watt, 1 min).

4. Remove PR by acetone and clean by piranha for 10 min.

Performing p+ doping
5. Deposit 900 nm SiO₂ by plasma enhanced chemical vapor deposition (PECVD; PlasmaTherm SLR).

6. Treat with hexamethyldisilazane (HMDS) for 2 min.

7. Pattern PR (Mask #2: P doping).

8. Bake at 110°C for 5 min.

9. Etch SiO₂ in buffered oxide etchant (BOE, 6:1) for 1.5 min.

10. Remove PR by acetone and clean by piranha for 10 min.

11. Expose to a boron doping source at 1000°C for 30 min.

12. Clean the processed wafer (concentrated (49%) HF 2 min, piranha 10 min, BOE 1 min).

**Performing n+ doping**

13. Deposit 900 nm SiO₂ by PECVD.

14. Treat with HMDS for 2 min.

15. Pattern PR (Mask #3: N doping).

16. Bake at 110°C for 5 min.

17. Etch SiO₂ in buffered oxide etchant (BOE, 6:1) for 1.5 min.

18. Remove PR by acetone and clean by piranha for 10 min.

19. Expose to a phosphorus doping source at 1000°C for 10 min.

20. Clean the processed wafer (HF 2 min, piranha 10 min, BOE 1 min).

**Releasing the top Si from SOI**

21. Pattern PR (AZ 5214) (Mask #4: Releasing hole 1).

22. Etch Si by RIE (50 mTorr, 40 sccm SF₆, 100 Watt, 3.5 min).

23. Remove PR by acetone and clean by piranha for 10 min.

24. Etch buried oxide layer in concentrated HF for 45 min.
25. Rinse and clean the processed wafer in DI wafer.

**Retrieving the Si film**

26. Bring a 6 mm thick PDMS (weight ratio of base: curing agent=10:1) stamp into contact with the Si.

27. Peel the stamp back to lift the Si film from SOI onto the stamp.

**Preparing the carrier wafer**

28. Spin cast polyimide (PI, poly(pyromellitic dianhydride-co-4,4’-oxydianiline) (4000 rpm, 30 sec) onto a 3”×2” glass slide.

29. Anneal at 150 °C for 10 min.

30. Anneal at 250 °C for 60 min in an N₂ atmosphere.

31. Deposit Cr/Au (5/300 nm) by electron beam evaporation (AJA International).

**Transfer printing the Si film**

32. Spin coat the carrier wafer with PI (4000 rpm, 30 sec).

33. Bake at 110 °C for 30 sec.

34. Bring the stamp with Si film on its surface into contact with the carrier wafer.

35. Bake at 110 °C for 30 sec.

36. Remove the PDMS stamp, leaving the Si on carrier wafer.

37. Anneal at 150 °C for 10 min.

38. Anneal at 250 °C for 60 min in N₂ atmosphere.

**Isolating the PIN heaters**


40. Etch Si by RIE (50 mTorr, 40 sccm SF₆, 100 Watt, 3.5 min).

41. Remove PR by acetone.


**Patterning metal to block light**

42. Pattern PR (AZ 4620, 3000 rpm, 30 sec) (Mask #6: Back light blocking metal).

43. Etch PI by RIE (MARCH, 300 mTorr, 150 Watt, 10 min).

44. Wet etch exposed Au/Cr for 54/7 sec.

45. Remove PR by acetone.

**Defining the via hole to the p contact**

46. Spin coat PI (4000 rpm, 30 sec).

47. Anneal at 150°C for 10 min.

48. Anneal at 250°C for 60 min in N₂ atmosphere.

49. Pattern PR (AZ 4620) (Mask #7: P via hole).

50. Etch PI by RIE (MARCH, 300 mTorr, 150 Watt, 10 min).

51. Remove PR by acetone.

**Defining the metal for the p contact**

52. Deposit Cr/Au (5/300 nm) by DC sputtering (AJA International).

53. Pattern PR (AZ 5214) (Mask #8: P metal).

54. Wet etch exposed Au/Cr for 54/7 sec.

55. Remove PR by acetone.

**Defining the via hole to the n contact**

56. Spin coat PI (4000 rpm, 30 sec).

57. Anneal at 150°C for 10 min.

58. Anneal at 250°C for 60 min in N₂ atmosphere.

59. Pattern PR (AZ 4620) (Mask #9: N via hole).

60. Etch PI by RIE (MARCH, 300 mTorr, 150 Watt, 20 min).
61. Remove PR by acetone.

**Defining the metal for the n contact**

62. Deposit Cr/Au (5/300 nm) by DC sputtering (AJA International).
63. Pattern PR (AZ 5214) (Mask #10: N metal).
64. Wet etch exposed Au/Cr for 54/7 sec.
65. Remove PR by acetone.

**Depositing PI encapsulation**

66. Spin coat PI (4000 rpm, 30 sec).
67. Anneal at 150°C for 10 min.
68. Anneal at 250°C for 60 min in N₂ atmosphere.

**Releasing the device**

69. Deposit 150 nm SiO₂ by PECVD.
70. Treat with HMDS for 2 min.
71. Pattern PR (Mask #11: Releasing hole 2).
72. Etch SiO₂ by RIE (50 mTorr, 40:1.2 sccm CF₄:O₂, 150 Watt, 8.5 min).
73. Remove PR by acetone.
74. Release device in BOE (6:1).

3. Fabricating the photodetector array and measuring its characteristics

Figure S7A shows an exploded schematic illustration of the layout of the Si, metal and PI layers associated with a single unit cell in the photodetector array. The major steps in the fabrication are similar to those for the heater array. Every unit cell in the photodetector array includes a photodiode and blocking diode constructed in a back-to-back configuration to eliminate crosstalk in passive matrix readout. In addition, the light sensitive intrinsic region of
the blocking diode is covered by a layer of Cr/Au to eliminate any response to light. Figure S7B shows the planar structure design of the photodetector. An optical image of the thin photodetector array appears in Fig. S7C. Detailed fabrication steps are as follows.

**Fabrication steps:**

*Defining alignment markers*

1. Clean 1.25 μm SOI wafer with acetone, IPA and DI water.
2. Pattern PR (AZ5214) (Mask #1: Alignment marker).
3. Etch Si by RIE (50 mTorr, 40 sccm SF6, 100 Watt, 1 min).
4. Remove PR by acetone and clean by piranha for 10 min.

*Performing p+ doping*

5. Deposit 900 nm SiO₂ by PECVD.
6. Treat with HMDS for 2 min.
7. Pattern PR (Mask #2: P doping).
8. Bake at 110°C for 5 min.
9. Etch SiO₂ in BOE (6:1) for 1.5 min.
10. Remove PR by acetone and clean by piranha for 10 min.
11. Expose to a boron doping source at 1000°C for 30 min.
12. Clean the processed wafer (HF 2 min, piranha 10 min, BOE 1 min).

*Performing n+ doping*

13. Deposit 900 nm SiO₂ by PECVD.
14. Treat with HMDS for 2 min.
15. Pattern PR (Mask #3: N doping).
16. Bake at 110°C for 5 min.
17. Etch SiO₂ in buffered oxide etchant (BOE, 6:1) for 1.5 min.

18. Remove PR by acetone and clean by piranha for 10 min.

19. Expose to a phosphorus doping source at 1000°C for 10 min.

20. Clean the processed wafer (HF 2 min, piranha 10 min, BOE 1 min).

**Releasing top Si from SOI**

21. Pattern PR (AZ 5214) (Mask #4: Releasing hole 1).

22. Etch Si by RIE (50 mTorr, 40 sccm SF₆, 100 Watt, 3.5 min).

23. Remove PR by acetone and clean by piranha for 10 min.

24. Etch buried oxide layer in concentrated HF for 45 min.

25. Rinse and clean the processed wafer in DI wafer.

**Retrieving the Si film**

26. Bring a 6 mm thick PDMS (weight ratio of base: curing agent=10:1) stamp into contact with the Si.

27. Peel the stamp back to lift the Si film from SOI onto the stamp.

**Preparing the carrier wafer**

28. Spin cast PI (4000 rpm, 30 sec) onto a 3”×2” glass slide

29. Anneal at 150°C for 10 min.

30. Anneal at 250°C for 60 min in N₂ atmosphere.

31. Deposit Cr/Au (5/300 nm) by electron beam evaporation.

**Transfer printing the Si film**

32. Spin coat the carrier wafer with PI (4000 rpm, 30 sec).

33. Bake at 110°C for 30 sec.

34. Bring the stamp with Si film on onto contact with the carrier wafer.
35. Bake 110°C for 30 sec.

36. Retrieve the PDMS stamp, leaving the Si on carrier wafer.

37. Anneal at 150°C for 10 min.

38. Anneal at 250°C for 60 min in N₂ atmosphere.

**Isolating the photodetectors**


40. Etch Si by RIE (50 mTorr, 40 sccm SF₆, 100 Watt, 3.5 min).

41. Remove PR by acetone.

**Patterning metal to block light**

42. Pattern PR (AZ 4620, 3000 rpm, 30 sec) (Mask #6: Back light blocking metal).

43. Etch PI by RIE (MARCH, 300 mTorr, 150 Watt, 10 min).

44. Wet etch exposed Au/Cr for 54/7 sec.

45. Remove PR by acetone.

**Defining via 1**

46. Spin coat PI (4000 rpm, 30 sec).

47. Anneal at 150°C for 10 min.

48. Anneal at 250°C for 60 min in a N₂ atmosphere.

49. Pattern PR (AZ 4620) (Mask #7: Via hole 1).

50. Etch PI by RIE (MARCH, 300 mTorr, 150 Watt, 10 min).

51. Remove PR by acetone.

**Depositing and patterning metal 1**

52. Deposit Cr/Au (5/300 nm) by DC sputtering (AJA International).

53. Pattern PR (AZ 5214) (Mask #8: Metal 1).
54. Wet etch exposed Au/Cr for 54/7 sec.

55. Remove PR by acetone.

**Patterning via 2**

56. Spin coat PI (4000 rpm, 30 sec).

57. Bake at 150 °C for 10 min.

58. Anneal at 250 °C for 60 min in N₂ atmosphere.

59. Pattern PR (AZ 4620) (Mask #9: Via hole 2).

60. Etch PI by RIE (MARCH, 300 mTorr, 150 Watt, 20 min).

61. Remove PR by acetone.

**Depositing and patterning metal 2**

62. Deposit Cr/Au (5/300 nm) by DC sputtering (AJA International).

63. Pattern PR (AZ 5214) (Mask #10: Metal 2).

64. Wet etch exposed Au/Cr for 54/7 sec.

65. Remove PR by acetone.

**Depositing PI encapsulation**

66. Spin coat PI (4000 rpm, 30 sec).

67. Anneal at 150 °C for 10 min.

68. Anneal at 250 °C for 60 min in N₂ atmosphere.

**Opening the bonding pad**

69. Cover the device with a 2 mm thick piece of PDMS and expose the bonding pad.

70. Etch the unprotected PI (MARCH, 300 mTorr, 150 Watt, 10 min) to expose the bonding pad.

**Releasing the device**

71. Deposit 150 nm SiO₂ by PECVD.
72. Treat with HMDS for 2 min.

73. Pattern PR (Mask #11: Releasing hole 2).

74. Etch SiO$_2$ by RIE (50 mTorr, 40:1.2 sccm CF$_4$:O$_2$, 150W, 8.5 min).

75. Remove PR by acetone.

76. Release device in BOE (6:1).

4. Fabricating and assembling the complete system

Assembling the complete system involves multiple steps of functional component fabrication and integration. Detailed fabrication steps are outlined in the following.

Fabrication steps:

**Bonding the heater array with thin PDMS**

1. Retrieve the thin heater array with a PDMS stamp.

2. Deposit 40 nm SiO$_2$ by PECVD.

3. Spin coat PDMS (10:1, 500rpm, 1 min) on a glass slide (2”×3”).

4. Bake at 80°C for 10 min.

5. Treat the front surface of the PDMS under a UVO lamp (BHK Inc.) for 5 min.

6. Bond the heater array with the treated PDMS.

**Constructing the artificial leucophor and chromatophore pixels**

7. Deposit Ag (300 nm) for the white background and heat spreading layer by electron beam evaporation.

8. Pattern PR (AZ 5214) (Mask #1: Ag).

9. Etch exposed Ag by wet etchants for 20 sec.

10. Remove PR by acetone.
11. Pattern the thermochromic composite by spin coating, pre-baking, exposing, post-baking and developing.

12. Clean with isopropyl alcohol (IPA) and deionized (DI) water.

**Opening the bonding pad for the heater**

13. Cover the device by a rectangular, ring-shaped piece of PDMS (2 mm thick) with a glass slide on top and expose the bonding pad.

14. Etch the unprotected PI (MARCH, 300 mTorr, 150 Watt, 10 min) to expose the bonding pad.

15. Peel off the PDMS with the heater and color changeable pixel array from the glass slide.

**Bonding the photodetector array**

16. Treat the back surface of the PDMS under a UVO lamp for 5 min.

17. Retrieve the photodetector array with a PDMS stamp.

18. Deposit 40 nm SiO$_2$ by PECVD.

19. Align and bond the photodetector array to the activated rear surface of the PDMS with all other components on the front side.

**5. Optical system and data acquisition**

Connecting the pins on a custom printed circuit board (PCB) that is interfaced to the devices, with control electronics and software enables background image acquisition, signal processing, and pulse power signal generation. Electronic diagrams for image acquisition are shown in Fig. S7D. The inputs and outputs, i.e. the columns and rows respectively, are interfaced with the control electronics of NI PXIe-6363 (National Instruments). The current responses at an applied bias of 3 V were measured for all the pixels in the 16 x 16 array, used to generate the image results of Fig. S8. Three different light intensities ranging from bright, working to complete darkness served to test the detector arrays. A good range of sensitivity is possible for the
photodetecting pixels, from current responses of 1100~1200 nA at the highest brightness to 0.5~3 nA in the dark state, as shown in Fig. 2C. The greyscale image of Fig. S8A represents the normalized photocurrent intensity map during image acquisition, while the binarized image by choosing the cut-off value of 0.25 was achieved as shown in Fig. S8B. The binarized data were used to control the pulse voltages to supply the heaters, thus to induce color change and pattern matching.

The circuit diagram of the heater array is shown in Fig. S5. Instead of directly interfacing the devices with the PXI control electronics, the heaters were powered using the output of a transistor (MCT2EM-ND, Fairchild Semiconductor Corp.) capable of meeting the power requirements. Figure S6 shows the controlling pulse (3 V) from the PXIe-6723 and the power supply pulse (12 V). The voltage directly applied to the heater pixel is 10.5 V, since there is some voltage drop on the two forward biased junctions from the circuit.

6. Moving background setup and device testing

The changeable background, which was used to verify the camouflaging capabilities, consisted of a backlight and a transparency mask. Specifically, diffusive light from an array of light emitting diodes (MB-BL4X4, Metaphase Technologies, Inc., USA) provided a uniform, white light illumination. The plastic transparency masks consist of various black patterns that block the light. Motion of this mask relative to the device system allowed demonstrations of dynamic change of the patterns. The schematic cartoons with various patterns are shown in Fig. 4. The whole setup was built on a stage to allow temperature control, with a set point of $T_0$. 
7. Thermal analysis

FEM, specifically the continuum element DC3D8 in the ABAQUS software(1), was used to study the temperature distribution in the device. The substrate, made of PI (thickness 9.95 μm) and PDMS (thickness 100 μm), was supported by a glass slide (thickness 1100 μm). As shown in Fig. S16A, the device consists of 16 × 16 pixels on the substrate, where each pixel consists of a layer of composite dye (thickness 65 μm) and Ag (thickness 0.3 μm) (Fig. S16B). The pixels have spacing of 100 μm, and in-plane dimensions of 820 × 820 μm² with four corners (each 110 × 110 μm²) removed (Fig. S16C). For each pixel, the PI layer underneath contains the (Si) heater and the gold layer with dimensions of 640 × 640 × 1.25 μm³ and 720 × 720 × 0.3 μm³, respectively (Fig. S2B). Figures S16 A and C also show Au interconnects between the heaters. The bottom of the glass slide has a constant temperature 40.5 °C, as in experiments. The entire top surface, and the lateral surfaces of pixels, have natural convection with the coefficient of heat convection of 5 W/(m²·K) and air temperature of 20 °C. Figure S16D illustrates the pulsed voltage of \( U_0 = 10.5 \) V and duration of \( t_0 = 17.5 \) ms in the period of \( T = 280 \) ms.

The thermal conductivity, heat capacity, and mass density are 0.2 W/(m·K), 1800 J/(kg·K), and 1200 kg/m³ for thermochromic dye(2, 3); 371 W/(m·K), 235 J/(kg·K), and 10492 kg/m³ for silver(4); 0.52 W/(m·K), 1090 J/(kg·K), and 1420 kg/m³ for PI(5, 6); 160 W/(m·K), 700 J/(kg·K), and 2329 kg/m³ for silicon(7); 317 W/(m·K), 129 J/(kg·K), and 19280 kg/m³ for gold(8, 9); 0.18 W/(m·K), 970 J/(kg·K), and 1460 kg/m³ for PDMS(7); 1.2 W/(m·K), 790 J/(kg·K), and 2700 kg/m³ for glass(10), respectively.

Figure S17A shows the temperature distribution, obtained by FEM, along the plane of the Si heaters (x direction) as illustrated in Fig. S17B, when all heaters are off except the center one, which receives pulsed power, and the temperature fluctuation is stabilized. The maximum
temperature increase in all heaters without power is only 3% of that in the center heater, which clearly demonstrates that the heat is well confined. Figure S18 shows that, during thermal fluctuation due to pulsed power, the maximum temperature on the surface of the heated pixel ranges from 57 to 65 °C. The temperature along z direction (normal to the surface) given in Fig. S19 suggests relatively uniform temperature across the thickness of the dye. Figure S20 compares the temperature distributions at the bottom surface of the dye, with and without the Ag layer. With Ag, the temperature is more uniform than that of the case of without Ag layer.

8. Mechanical analysis

This analysis of strains and stresses in the device during bending by FEM upon application of a load along the x and y directions is performed. The thermochromic composite dye and PDMS are modeled as three-dimensional solids. The multilayer structures consist of metal, silicon and PI, are modeled as shells. The Young’s modulus and Poisson’s ratio are 130 GPa and 0.27 for silicon, 78 GPa and 0.44 for Au, 2 MPa and 0.49 for PDMS and 2.5 GPa and 0.34 for PI, respectively. Figure S12B captures the maximum strain in the silicon for bending to different bending radii.
References


Supplementary Movie Legends

Movie S1. Experimental thermal movie of camouflaging of a digital pattern “O”.

Movie S2. FEM thermal movie of camouflaging of a digital pattern “O”.

Movie S3. Movie of dynamic, adaptive pattern recognition and color camouflaging against a moving square background. The video is sped up by 3 times.

Movie S4. Movie of dynamic, adaptive pattern recognition and color camouflaging on a changing background. The video is sped up by 3 times.

Supplementary Figure Legends

Figure S1. (A) Optical image of the black thermochromic slurry at room temperature, ~22°C. (B) Optical image of the slurry at 47°C. At this temperature, the slurry is transparent, thereby a background picture underneath is visible. (C) SEM image of an array of photopatterned thermochromic pixels. (D) SEM image of the top surface of a patterned pixel. (E) Optical image of the pixel arrays (16×16) at room temperature of 22°C. (F) Optical image of the arrays (16×16) at 47°C.

Figure S2. (A) Exploded schematic illustration of the layout of the Si, metal, and PI layers of a single pixel in the heater array. (B) Optical image of the Si diode. The dark dots represent the releasing holes etched through the Si. (C) Optical image of the heater array. (D) Thermal image of the array with one pixel activated. The heat is mostly confined within the area of the activated heater, with minimal changes in neighboring pixels. The background temperature was set to 30°C.
Figure S3. Schematic illustration of the major steps for fabricating flexible devices based on Si nanomembranes. (A) Preparing the device elements by selective doping. (B) Opening holes and undercut etching in concentrated HF. (C) Retrieving the Si from the SOI wafer using a PDMS stamp. (D) Printing the Si onto a glass substrate with a thin layer of PI. (E) Peeling away the stamp to leave the Si on the glass. (F) Patterning the Si and completing the metallization and passivation steps. (G) Releasing the flexible device from the glass.

Figure S4. (A) Optical images of a diode heater with P⁺ and N⁺ doping regions on an SOI wafer. (B) Optical image of a 1.25 μm thick Si membrane on a PDMS stamp. (C) Optical image of the Si membrane transfer printed onto a glass substrate which was coated with PI. (D) Optical image of a flexible array of diode heater held by a tweezer.

Figure S5. Schematic circuit diagram of a heater array and its external circuits.

Figure S6. Images of representative pulse signals. (A) The green curve is the control signal generated with a program created in Labview. The yellow curve is the output pulse applied to the heater. (B) Magnified image of both curves.

Figure S7. (A) Exploded schematic illustration of the layout of the Si, metal, and PI layers of a single pixel in the photodetector array. (B) Schematic illustration of the photodiode and blocking diode. (C) Optical image of the thin flexible photodetector array folded on a glass slide. (D) Schematic circuit diagram of the photodetector array.
Figure S8. (A) Normalized photocurrent intensity map associated with a digital pattern in the geometry of the text “UIUC MRL”. (B) Corresponding binarized intensity map.

Figure S9. Schematic steps for assembling the entire system. (A) Schematic illustration of a unit cell of the heater array and a thin PDMS substrate, prior to bonding. (B) Illustration of the bonded device. (C) Illustration of the Ag pixel fabricated on the device. (D) Illustration of a unit cell of the thermochromic pixel on top of the Ag pixel and the photodetector to be bonded together. (E) Illustration of the integrated system.

Figure S10. (A) Optical image of the heater array on a PDMS substrate. (B) Optical image of the Ag pixels fabricated on the heater array. (C) Optical image of the heater array and Ag pixels viewed from the backside.

Figure S11. Optical image of the device with ACF cable and custom made PCB with pin connectors.

Figure S12. (A) FEM model of the system, showing a 5x5 array. (B) FEM results of the maximum strain in the Si within the device at different bending radii. The red dots are the results for bending along x axis. The blue dots are the results for bending along y axis.

Figure S13. (A-H) IR images of the device when one pixel is actuated, as the actuation voltage increases from 5.5 V to 12.5 V, with an increment of 1 V.
Figure S14. (A-D) IR images of the device when 8 pixels (digital pattern of “o”) are actuated, as the actuation voltage increases from 8.5V to 11.5V, with the increment of 1V.

Figure S15. (A) IR image of the heater array with one pixel activated at 10.5V. The arrow points to the geometrical center of the pixel. (B) Temperature fluctuation at the center of the pixel. The power was turned on and off at 11 s and 41 s, respectively. (C) Temperature information during the period of 20~30 s, as highlighted by the red dotted rectangular in (B).

Figure S16. (A) FEM model for the thermal analysis. (B) Cross-sectional (front) view of the pixel with the key dimensions. (C) Top view of the pixels. (D) Schematic pulse input for the FEM simulation.

Figure S17. (A) FEM results of the temperature within the layer of the Si heater arrays. The red curve shows the maximum temperature, and the black curve represents the minimum temperature. The results clearly show good heat confinement within the region of the activated pixel. (B) Schematic cross-sectional view of the heater layer.

Figure S18. (A) FEM results of the temperature along the x axis of the pixel. The black curve shows the maximum temperature, and the red curve represents the minimum temperature. (B) Schematic cross-section view of the heater.

Figure S19. (A) FEM results of the temperature across the thickness of the device. The black curve shows the maximum temperature, and the red curve represents the minimum temperature.
Figure S20. (A) FEM results of the temperature along the $x$ axis of the pixel for the cases with and without Ag heat spreading layer. The black curve shows the maximum temperature with the Ag, and the red curve shows the maximum temperature without Ag. The temperature is more uniform across the whole pixel with Ag. (B) Schematic cross-sectional view of the heater pixel.
Selective doping on SOI wafers.

Open releasing holes, undercut etching.

Apply rubber stamp; peel back stamp to grab objects.

Apply “inked” stamp to receiving substrates.

Transfer printing to a receiver substrate for processing.

Isolation, metallization and passivation.

Releasing device from substrate.
Heater pixels

Column scan; pulse input

P1  P2  P3  P4

Transistor

Heater pixels

Row control

Vcc

Figure S5
Normalized intensity

Binarized intensity

0 if ≤ 0.25; 1 if > 0.25.

Figure S8
Figure S9

A. Heater

B

C. Ag

D. Thermochromic dye

E. Photodetector
Pins to connect to external cable out for environmental viewing

Heater power input connection

1 cm

Figure S11
Figure S12

Maximum Strain in Silicon (%)

Bending radius (mm)

Bending along x axis

Bending along y axis

A

B

Maximum Strain in Silicon (%)

Bending along x axis

Bending along y axis

2

4

6

8

10

0.2

0.4

0.6

0.8

0

0.2

0.4

0.6

0.8

2

4

6

8

10

Bending radius (mm)
Figure S13
Figure S15

A

Temperature plot

B

Power on

Temperature (°C)

Time (s)

Power off

C

Time (s)

Temperature (°C)
Figure S18
Figure S19
Figure S20

A

Temperature (°C)

$\begin{align*}
\text{Temperature (°C)} \\
\text{x (μm)}
\end{align*}$

With Ag
Without Ag

B

Dye
Silicon heater
PDMS

$\text{A}$

$\text{B}$

Figure S20
Supporting Information

Yu et al. 10.1073/pnas.1410494111

Movie S1. Experimental thermal movie of camouflaging of a digital pattern “O.”

Movie S2. FEM thermal movie of camouflaging of a digital pattern “O.”
Movie S3.  Movie of dynamic, adaptive pattern recognition and color camouflaging against a moving square background. The video is sped up by three times.

Movie S4.  Movie of dynamic, adaptive pattern recognition and color camouflaging on a changing background. The video is sped up by three times.

Other Supporting Information Files

SI Appendix (PDF)